

International Journal of Advanced Research in Science, Engineering and Technology

Vol. 7, Issue 10 , October 2020

# Separation of Phases Formed During the Process of Desfluorization of Extraction Phosphoric Acid with Sodium Phosphates

Khodjamkulov S.Z.,Khujamberdiev Sh.M.,Melikulova G.E., Mirzakulov Kh.Ch.,Shaymardanova M.A.

Assistant Professor, Department Industrial Technology, Termez State University. Termez, Uzbekistan Assistant Professor, Department Chemical Technology of Inorganic Substances, Tashkent Institute of Chemical Technology. Tashkent, Uzbekistan

Junior Researcher, Department Chemical Technology of Inorganic Substances, Tashkent Institute of Chemical Technology. Tashkent, Uzbekistan

Professor, Department Chemical Technology of Inorganic Substances, Tashkent Institute of Chemical Technology. Tashkent, Uzbekistan

PhD Student, Department Chemical Technology of Inorganic Substances, Tashkent Institute of Chemical Technology. Tashkent, Uzbekistan

**ABSTRACT:** The article provides data on the development of a technology for defluorinating extraction phosphoric acid from phosphorites of the Central Kyzylkum using sodium phosphates, followed by phase separation and filtration of the sediment. The possibility of practically complete defluorination of the extraction phosphoric acid and obtaining a transparent acid is shown. Under these conditions, a fairly loose, well-filterable precipitate is formed.

**KEY WORDS:** Extraction Phosphoric Acid, Sodium Phosphate, Defluorination, Filtration, Sediment, Phase Separation, Precipitant, Sedimentation Rate.

### I. INTRODUCTION

In Uzbekistan, serious attention is paid to the problems of environmental protection from large-tonnage man-made, household waste, protection of soil, water resources from the ingress of various chemical and harmful substances into them [1-4].

#### **II. LITERATURE REVIEW**

At the enterprises of the chemical industry, more than 700 thousand tons of phosphorites of the Central Kyzylkum (CK) are annually processed into extraction phosphoric acid (EPA) and phosphorus-containing fertilizers [5-7]. The content of fluorine in phosphorus-containing fertilizers produced in the republic, such as ammophos, PS-Agro, suprephos, enriched superphosphate, ranges from 2 to 4%. This is due to the fact that during sulfuric acid decomposition of CK phosphorites, 40.5% of fluorine passes into the gas phase, 5.4% is removed with phosphogypsum, and 54.1% remains in the EPA [8]. The low solubility of fluorine compounds in the composition of mineral fertilizers in a large sea prevents the removal of fluorine from the soil by thawed, rain and irrigation waters, as well as assimilation by plant organisms. However, the annual increase in the amount of applied mineral fertilizers, the use of chemical plant protection products, defoliants can change the solubility of fluorine compounds to the formation of assimilable forms by plants and animals. Many plants are capable of accumulating significant amounts of fluoride. So, tea contains from 57 to 1370 mg of fluorine per 1 kg, and in cotton plant up to 400 mg [4, 9, 10]. Moreover, fluoride accumulates in cotton seeds. The amount of fluoride absorbed by plants increases with the use of NPK fertilizers [3]. The intake of an excess amount of fluoride is negative not only on plants, but also on humans, animals, and fish. Fluorine compounds in water and air, even in small quantities, have a very harmful effect on living organisms [11-13].

On the other hand, fluorine compounds are a valuable chemical raw material and, despite the ever-increasing needs of the world economy for fluorine compounds, at present they are practically not extracted and remain in the composition



## International Journal of Advanced Research in Science, Engineering and Technology

#### Vol. 7, Issue 10, October 2020

of mineral fertilizers. Therefore, studies aimed at processing CK phosphorites to obtain defluorinated EPA, which allows solving economic and environmental problems - reducing the content of fluoride in fertilizers and obtaining fluoride salts are very topical and relevant.

#### **III. RESEARCH METHODOLOGY**

For the conditions of Uzbekistan, the most acceptable method for defluorination of EPA is the sedimentation of fluorine compounds from acid with sodium compounds in the form of sodium silicofluoride [14-17].

One of the bottlenecks in the defluorination process is the separation of the precipitate of silicofluorides, since they are deposited in the form of small crystals with a highly developed specific surface. The data available in the literature on the study of the processes of sedimentation of silicofluorides and or the stable part of EPA, depending on various parameters and the ways of intensifying the separation of solid and liquid phases, are not sufficient for the development of an effective technology for obtaining defluorinated EPA.

The required amount of alkali metals for defluorination was calculated based on the 6F : 2Na ratio. The rate of alkali metals was varied from 100 to 200% of the stoichiometry for the formation of sodium silicofluoride.

In this regard, the influence of the rate of an alkaline precipitant, the required amount of alkali metals for defluorination, addition of phosphorite, the ratio of Na<sub>2</sub>O in a solution of sodium salts on the sedimentation rate of particles and the filtration rate of the precipitate formed during defluorization of EPA was studied. In the work used industrial EPC of Almalyk JSC "Ammophos-Maxam" composition (wt.%):  $P_2O_5 - 22.4$ ; F - 1.2; SO<sub>3</sub>w - 2.2;  $R_2O_3 2.3$ ;  $R_2O - 0.4$  and suspensions 2.5. Experiments on the defluorination of EPA were carried out in a laboratory setup consisting of a glass reactor equipped with a stirrer.

In order to intensify the processes of decantation and filtration, we used a precipitant - CaSO<sub>4</sub>•2H<sub>2</sub>O, formed by the interaction of free sulfuric acid contained in EPA with phosphate raw materials. The amount of the latter was varied in the range of 0-120% of the stoichiometry for the formation of calcium sulfate dihydrate. At the same time, it was assumed that the resulting CaSO<sub>4</sub>•2H<sub>2</sub>O crystals have sufficient size and density, in comparison with the CaF<sub>2</sub>, Ca<sub>5</sub>F(PO<sub>4</sub>)<sub>3</sub>, Na<sub>2</sub>SiF<sub>6</sub> and SiO<sub>2</sub> particles formed in the extraction suspension, and that large crystals during deposition should capture smaller particles in solid phase. It is known that the greatest effect of the precipitant follows at the moment of its formation [18]. Therefore, in the experiments, special conditions were created for the formation of CaSO<sub>4</sub>•2H<sub>2</sub>O. This was achieved by mixing phosphorite with the original EPA at a temperature of 70°C for 40 minutes. in a thermostated reactor. The resulting suspension was poured with stirring into measuring cylinders with a capacity of 100 cm<sup>3</sup>. The deposition time was recorded when a sufficiently clear phase boundary was reached. The sedimentation rate (W, m/h), the L:S ratio in the suspension (L:S), and the filterability (F) were determined by a known method [19]. The deposition rate was calculated using the formula:

$$W = \frac{l \cdot 60}{\tau}$$

where, *l*-path covered in time  $\tau$ , min. The L:S ratio in the suspension was calculated using the equation:

$$L: S = \left(\frac{j_p}{j_L} - 1\right): \left(1 - \frac{j_L}{j_S}\right)$$

where,  $j_P$ ,  $j_L$ ,  $j_S$  - the specific gravity of the pulp, liquid and solid phases, respectively. Filterability was determined by the formula:

$$F = \frac{V_F * h_{sed}}{\Delta P * S * \tau}$$

where, F - filterability,  $m^4/H$ ·hour;  $V_F$  - filtrate volume,  $m^3$ ;  $h_{sed}$  - is the thickness of the filter cake layer, m;  $\Delta P$  - pressure difference,  $N/m^2$ ; S - filter area,  $m^2$ ;  $\tau$  - filtration duration, hour.

The average density of the solid phase, consisting of particles  $CaSO_4 \cdot 2H_2O$ ,  $CaF_2$ ,  $Ca_5F(PO_4)_3$ ,  $Na_2SiF_6$ ,  $SiO_2$ , etc., is equal to 2450 kg/m<sup>3</sup>.

Filtration of suspensions was carried out on a Schott filter with a porosity of 100  $\mu$ m at a vacuum of 75-80 kPa. The precipitate was washed with hot water, acetone, dried at a temperature not exceeding 60°C and weighed. The filtration time was recorded by the appearance of a sediment mirror.



## International Journal of Advanced Research in Science, Engineering and Technology

## Vol. 7, Issue 10, October 2020

### IV. ANALYSIS AND RESULTS

The initial EPA in the absence of phosphorite and a solution of alkali metal phosphates clears up rather quickly, but the upper acid layer, after the precipitation of the bulk of the sediment, remains cloudy and contains a significant amount of fine silty, suspended particles for a long, more than 10 hours, settling. The addition of an insignificant amount of CK phosphorite ( $N_{ph/r}$  50% of stoichiometry on SO<sub>3</sub>) at a mass ratio of EPA: phosphate raw material - 100:(0.6-1.2) allows to drastically reduce the sulfate content in acid by almost 2 times (table 1).

The upper acid layer after settling, in contrast to the initial EPA, is noticeably lighter, which is due to the crystallization of calcium sulfate on suspended particles and their coprecipitation into the solid phase. The sludge mass increases by 1.7 times with an almost unchanged height of the clarified layer, which indicates a significant sludge compaction.

Table 1. Influence of the phosphorite rate on the degree of sedimentation of suspensions during defluorization and desulfurization of EPA (process duration - 40 min; process temperature - 70°C; settling time - 120 min; settling temperature - 30°C

Experimen	Phosphate	Height of	Filtration	Sediment	L:S ratio in	L:S ratio in	Defluorination	Degree of	
t number	raw	the	rate,	yield (per	suspension	thickened	degree	desulfurization	
	material	clarified	kg/m <sup>2</sup>	100 g of		suspension	%	niya,%	
	rate,%	layer,%		EPA)					
Without alkali metals									
1	-	87,4	170,49	1,78	55,18:1	6,95:1	13,85	0	
2	25	83,1	182,50	2,40	40,98:1	6,92:1	14,72	30,01	
3	50	82,7	254,44	3,01	32,63:1	5,65:1	16,34	47,84	
4	75	66,7	250,80	3,65	26,91:1	8,69:1	22,33	66,70	
5	100	65,0	245,41	4,70	20,80:1	7,28:1	23,50	91,20	
6	120	60,7	230,24	5,28	18,50:1	7,26:1	24,00	95,00	
In the presence of alkali metals in a solution $\sum R2O:\sum P = 1:1$									
7	-	80,00	110,12	2,78	40,85:1	10,86:1	71,28	0	
8	25	69,24	121,30	4,10	27,52:1	9,71:1	73,59	33,00	
9	50	58,50	168,91	5,40	20,77:1	9,51:1	75,87	52,50	
10	75	57,91	180,40	6,77	16,46:1	7,31:1	77,83	68,00	
11	100	53,50	178,91	7,35	13,94:1	6,95:1	82,87	95,90	
12	120	49,50	170,12	8,28	13,44:1	7,19:1	83,30	96,00	

This is confirmed by the ratio L:S in the thickened part of the suspension, which is (5.5-10.86):1.

An increase in the amount of added phosphorite ( $N_{ph/r}$  - 75-100%) leads to almost complete defluorination of EPA and the production of a transparent acid. Under these conditions, a fairly loose, well-filterable precipitate is formed, represented mainly by calcium sulfate dihydrate with an insignificant amount of silica, which contains CK in phosphorite.

An increase in  $N_{ph/r}$  above stoichiometry practically does not contribute to further desulfurization, but leads to a sharp deterioration in the process of decantation and filtration of the sediment. This is due to the fact that in the process of interaction of excess phosphorite with phosphoric acid, the latter extracts Ca, Mg, Fe and Al cations into solution, increasing the viscosity of the acid, and the insoluble phosphorite precipitate with poor filtering properties dilutes well-filterable gypsum.

A similar picture is observed with the simultaneous addition of sodium phosphate solution to the initial EPA for defluorination and phosphorite (table 1).

In the absence of phosphorite, despite the fact that the phase separation occurs rather quickly, a poorly filterable, finely dispersed precipitate of silicofluorides in a mixture with suspended particles of the original EPA is formed. The clarified part remains cloudy for a day or more, although the content in it is no more than 0.2-0.3 mass. The filtration rate of such a sediment does not exceed  $110.12 \text{ kg/m}_2 \cdot h$ .

Adding, together with a solution of alkali metal phosphates, phosphate rock in an amount of 75-100% of the stoichiometry for binding  $SO_3$ , it is possible to significantly increase the degree of defluorination (by 7-10 abs.%) and desulfurization to 70-90% (table 1). The filtration rate of the sediment increases by more than 1.5 times compared to the precipitate obtained without adding phosphorite. The liquid phase is transparent, does not contain suspended



# International Journal of Advanced Research in Science, Engineering and Technology

#### Vol. 7, Issue 10, October 2020

particles, it is easily separated from the thickened part without agitation, despite the fact that L: S in suspension is (16.5-14.1):1. The thickened part is characterized by an almost optimal ratio of L:S, equal to (7.0-7.4):1, which makes it possible to carry out the subsequent processing of the precipitate into a solution of sodium phosphates and concentrated fluorine-containing gases without additional processing.

The indices of the process of defluorination and subsequent thickening of the suspension and filtration of the precipitate significantly depend on the composition of the precipitate, which is determined by the composition of the precipitation solution and the  $\sum Na2O: \sum (F_{EPA} + F_{ph'r})$  ratio (table 2).  $\sum Na_2O = Na_3PO_4 + Na_2SiO_3$ , the content of acid-soluble silicon in EPA obtained from CK phosphorites is insufficient for the complete conversion of all fluorine into sodium silicofluoride, which causes a low degree of defluorination [1]. In this regard, experiments were carried out on the defluorination of EPA with sodium salts in the presence of sodium silicate in order to correct the ratio of SiO<sub>2</sub>:F in EPA.

Table 2. Influence of norm, concentration of alkali metal (Na<sub>2</sub>O) on the process of sedimentation of suspensions during defluorination of EPA (process temperature - 70°C; process duration - 40 min; settling temperature - 30°C; settling time - 120 min; N<sub>ph/r</sub> = 75%).

Experience	Mass	Height of the	Sedimentation	L:S ratio in the	L:S ratio in a	Sediment	Filtration rate,
number	ratio	clarified	rate, m/h	initial	thickened	yield,%	kg/m <sup>2</sup> ·h
	Na <sub>2</sub> O:F	layer, %		suspension	suspension		
1	0,4:1	47,2	1,07	18,82:1	8,13:1	5,85	98,8
2	0,6:1	51,7	1,27	18,43:1	8,53:1	6,06	120,8
3	0,8:1	54,3	1,38	18,09:1	8,83:1	6,35	165,3
4	1:1	54,3	1,39	17,96:1	8,86:1	6,58	176,7

As can be seen from the presented data, all other things being equal, an increase in  $\sum Na_2O:\sum F$  from 0.4:1 to 1:1 leads to an insignificant increase in the filtration rate of the sediment with a simultaneous compaction of the sediment (table 2). The height of the clarified layer with a decrease in L:S and an increase in the yield of the solid phase increases by 5-11%. Moreover, these indicators are significantly improved when using sodium phosphate solutions for fluorine precipitation. The filtration rate of the precipitate when defluorinated with a solution with a mass ratio of Na<sub>2</sub>O: $\sum F$ equal to 1:1 is 176.7 kg/m<sup>2</sup> h.

Taking into account that in real technological conditions the sedimentation temperature is directly dependent on the ambient temperature and fluctuates in the range of 20-60°C, the effect of temperature on the sedimentation and filtration rate of the sediment formed during desulfurization and defluorination of the EPA CK was studied (table 3).

Table 3. Influence of sedimentation temperature on the process of suspension sedimentation during defluorination ofEPA (duration - 40 min, phosphorite rate - 75%, sedimentation time - 120 min.)

Experienc e number	1	Height of the clarified	Sediment ation	Sediment yield, %	L:S ratio in suspension	L:S ratio in a thickened	Filtration rate, kg/m <sup>2</sup> ·h
1	e, °C 20	layer, % 59.2	rate, m/h 1,29	7.0	16,01:1	suspension 7,16:1	178,2
2	40	60,4	1,58	6,5	17,31:1	7,57:1	209,45
3	50	60,9	1,67	6,2	18,29:1	7,88:1	307,57
4	60	61,0	1,68	6,2	18,31:1	7,90:1	309,41

With an increase in temperature from 20 to 60°C, the rate of sedimentation of the solid phase and the rate of filtration of the sedimente slightly increase from the used solution of alkali metal phosphates. For example, at 20°CW<sub>sed</sub> is 1.29 m/h, and at 60°C it reaches 1.68 m/h, and the filtration rate of the sediment increases from 178.2 to 309.41 kg/m<sup>2</sup> h. At a temperature of 50°C, the bulk of the particles, up to 97-98%, settles in the first 30-40 minutes, and at 20°C within 2-2.5 hours.

A significant difference in the rate of sedimentation of particles and filtration of the sediment with an increase in the settling temperature is due to a sharp decrease in the density and, especially, in the viscosity of the liquid phase of the suspension with increasing temperature.

Under optimal process conditions, the maximum sedimentation rate of solid phase particles is 2 m/h with a degree of defluorination and desulfurization of 73-89 and 70-95%, respectively.



## International Journal of Advanced Research in Science, **Engineering and Technology**

#### Vol. 7, Issue 10 , October 2020

#### VI. CONCLUSION

Thus, the addition, together with the solution of alkali metal phosphates, of the CK phosphate raw material in an amount of 75-100% of the stoichiometry for  $SO_3$  binding makes it possible to significantly increase the degree of defluorination by 7-10% and desulfurization to 70-90%. The filtration rate of the sedimentate increases by more than 1.5 times in comparison with the precipitate obtained without the addition of phosphorite. With an increase in temperature from 20 to 60°C, the sedimentation rate of the solid phase and the filtration rate of the sediment slightly increase.

#### REFERENCES

1. National report on the state of the environment and the use of natural resources in the Republic of Uzbekistan - 2008. (Retrospective analysis for 1988-2007). / Under. ed. Alikhanova B.B. - Tashkent: Chinor ENK, 2008. - 298 p.

2. Extent and economic consequences of fluoride pollution. Survey information. Issue 1. Obninsk, Russia. 1983. 55 p.

3. Lyubashevsky N.M., Turner V.I., Shcherbakov S.V. Technogenic pollution of the environment with fluorine. - Yekaterinburg, Russia. 1996. - 238

4. Vasyaev G.V., Markova A.G. Changes in the quality of agricultural products when fluoride enters the soil with mineral fertilizers. // Notes of the Leningrad s.-kh. in-that. L.: Publishing house of Leningrad Agricultural Institute, 1974, T. 245, - pp. 43-49.

5. Beglov B.M., NamazovSh.S. Phosphorites of Central Kyzylkum and their processing. Tashkent, Uzbekistan, 2013, 460 p.

6. Mirzakulov Kh.Ch. Physico-chemical foundations and technology for processing phosphorites of the Central Kyzylkum. // Ed. "Tafakkur", ISNB Tashkent, Uzbekistan, 2019, 412 p.

7. Volynskova N.V. Development and improvement of technology for the production of extraction phosphoric acid from phosphorites of the Central Kyzylkum. // Diss. ... doc. thech. sciences, - Tashkent, Uzbekistan, 2019, 270 p.

8. Shamshidinov I.T. Development of an improved technology for the production of extraction phosphoric acid and the production of concentrated phosphorus-containing fertilizers from phosphorites of Karatau and Central Kyzylkum. // Diss. ... doct. thech. sciences, - Tashkent, Uzbekistan, 2019, 193 p.

9. Pavlov I.N. Woody plants in conditions of technogenic pollution. Ulan-Ude. "The science". - 2005, 116 p.

10. Resolution of the cabinet of ministers of the Republic of Uzbekistan on the approval of the environmental monitoring program in the Republic of Uzbekistan for 2016-2020. Tashkent, 23 August 2016, No. 273.

11. Pafenova A.P., Ekimova O.A. Pollution of small rivers of the Sverdlovsk region as an indicator of sustainable development of the territory. Proceedings of the VI International Scientific and Practical Conference 2018. Yekaterinburg, Russia. - pp. 227-235.

12. Sadilova M.S., Petina A.A. Effects of inhalation of air containing fluoride by animals. Hygiene and sanitation. Russia, 1990, No. 8. - pp. 14-17.

13. Middle V.P. Soil contamination. - Tomsk, Russia, Tomsk State University Publishing House. 2015, 346 p.

14. Khodjamkulov S.Z., Nomozov A.K., Melikulova G.E., Mirzakulov Kh.Ch. Investigation of defluorination of extraction phosphoric acid obtained from the thermoconcentrate of the Central Kyzylkum. // "Universum" technical science scientific journal. Moscow, Russia, 2019. 2 (59), - pp. 93-96. 15. Khodjamkulov S.Z., Melikulova G.E., KhujamberdievSh.M., Mirzakulov Kh.Ch. Research of the process of decomposition of extraction phosphoric acid by sodium carbonate in the presence of sodium silicate // International Journal of Advanced Research in Science, Engineering and Technology // Vol. 7, Issue 9, September 2020 [ISSN: 2350-0328]. pp. 14912-14916.

16. El-Asmy A.A., Serag H.M., et al. Purification of phosphoric acid by minimizing iron, copper, cadmium and fluoride // Separation and Purification Technology. – 2008. – Vol. 61. – No. 3. – pp. 287-292.

17. Khodjamkulov S.Z., Mirzakulov Kh.Ch., Melikulova G.E., Usmanov I.I. Investigation of the process of defluorination of extraction phosphoric

acid from phosphorites of the Central Kyzylkum // Journal "Chemistry and Chemical Technology". Tashkent, Uzbekistan. 2020, No. 2. - pp. 36-39. 18. Khodjamkulov S.Z. Development of technology for defluorination of extraction phosphoric acid from the thermoconcentrate of the Central Kyzylkum to obtain sodium and calcium fluorides // Diss. ... cand. thech. sciences. - T.: 2009. 136 p.

19. Zhuzhikov V.A. Filtration. Theory and practice of suspension separation. - M.: Chemistry, 1980. 4th ed. 400 p.